NUCLEAR DATA EVALUATION FOR JENDL **ACTINIDE** FILE AND HIGH ENERGY DATA FILES

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ABSTRACT

Evaluation of nuclear data for JENDL Actinide File and High Energy Files is now in progress. JENDL Actinide File will contain evaluated nuclear data for 89 nuclides from 2 0 8 - to $^{255}{\rm Fm}$ including main fissile and fertile nuclides. The data are evaluated in the neutron energy region from $10^{\circ s}{\rm eV}$ to 20 MeV, by widely using theoretical calculations and systematic of parameters and cross sections. Evaluation of high-energy neutron and charged particle nuclear data has been initiated to make high energy data files of nuclides related to an accelerator–driven spallation system and a neutron irradiation facility of ESNIT. So far, the evaluation of neutron and proton-induced reaction data of $^{27}{\rm Al}$, Pb and $^{209}{\rm Bi}$ has been finished up to 1.0 GeV by mainly using the ALICE-F code and associated programs based on systematics. This paper describes their evaluation methods and status of these files.

I. INTRODUCTION

Management of high-level radioactive nuclear waste from nuclear reactors is one of the most important research subjects in the nuclear fuel cycle. In 1988, Japan decided to promote the OMEGA (Options Making Extra Gains of Actinides and fission products generated in nuclear fuel cycle) project. One of the possible options of radioactive waste management is to convert the long—lived radioactive nuclides to stable or short-lived ones by using nuclear transmutation reactions. Japan Atomic Energy Research Institute (JAERI) is investigating two ideas of such nuclear transmutation systems.

In the first process of the both ideas, the high-level radioactive waste is partitioned by chemical processing into 4 groups: minor actinides (Np, Pu, Am, Cm, etc.), Tc-Platinum group (Tc, Ru, Rh, Pd, etc.), Sr-Cs elements (Sr and Cs), and other nuclides (Zr, Mo, etc.). A current target of the nuclear transmutation is the minor actinides separated from the waste. An actinide burner fast reactor¹ is one of the ideas, in which the minor actinides are mainly transmuted by the fission, capture and (n,2n) reactions with a neutron spectrum harder than normal fast reactors. Another idea is an accelerator-driven spallation system² with a high intensity and high energy proton accelerator and a subcritical assembly of minor actinides. In this system, the transmu-

tation is mainly caused by chain reactions in the sub-critical assembly with source neutrons generated by the **spallation** reactions with target materials such as tungsten, lead and bismuth.

For the actinide burner reactor, in addition to the nuclear data of main fissile, fertile and structural material nuclides, the data of minor actinides are important, in particular, their fission, capture and (n,2n) reaction cross sections, the number of neutrons per fission and fission product yield data for the neutrons below 20 MeV. Data of main actinide nuclides in available evaluated nuclear data libraries such as JENDL-3, ENDF/B-VI, JEF-2, are accurate enough in the energy range below 20 MeV. However, those of the minor actinides are neither accurate enough, nor given in the current evaluated nuclear data libraries.

As one of JENDL (Japanese Evaluated Nuclear Data Library) special purpose files, the JENDL Actinide File is being made to meet the data requirements for the **actinide** burner reactor, and to provide reliable nuclear data for estimation of amount of **nuclides** generated in the nuclear reactors. The evaluation work for the JENDL Actinide File is described in Chapter 11.

The research and development of the accelerator-driven spallation system need the proton- and neutron-incident nuclear data in the energy region up to a few GeV for structural material, spallation target and nuclides to be transmuted. In this energy region, no evaluated nuclear data is available, except for only a few nuclides. Necessary data are double differential cross sections (DDXs) for the emitted particles, isotope production cross sections and the data related to high energy fission. The DDXS are important to calculation of secondary interactions in the materials, particle transportation, shielding design, etc. The isotope production cross sections are necessary to estimate the residual radioactivity.

In addition, the project of Energy Selective Neutron Irradiation Test Facility (ESNIT)³ is under way in JAERI, which is an FMIT type d-Li neutron source. For design of ESNIT, the nuclear data of structural materials are required up to 50 MeV because of the high energy tail of d-Li neutrons.

High energy data files are being planned to provide the data for **ESNIT** and the accelerator-driven **spallation** system. The tile for **ESNIT** will contain the neutron-induced reaction data up to 50 MeV. The other file for the accelerator-driven **spallation** system provides the neutron- and proton-induced data of the above-mentioned quantities of all the kinds of **nuclides** needed such as structural materials and candidates of **spallation** targets in the energy region up to 1.5 GeV. Chapter 111 is devoted to description of the high-energy data files.

II. EVALUATION FOR JENDL ACTINIDE FILE

The JENDL Actinide File will contain the evaluated data for 89 nuclides from ^{208}Tl to ^{255}Fm , in the neutron energy region from 10°eV to 20 MeV. The nuclides were selected on the basis of the following considerations:

- 1) **nuclides** from Th to Es with a half-life longer than 1 day.
- nuclides on the 4 major decay paths of actinides, with a halflife longer than 1 day.
- 3) nuclides whose data are already stored in JENDL-3.
- 4) some exceptional nuclides.

Table 1 lists the 89 nuclides to be stored in the JENDL Actinide File. The nuclides having high priority in the actinide burner reactor are marked with "A" or "B". "A" indicates major actinides, and "B" important minor actinides for design of the actinide burner reactor. The data for 57 nuclides marked with "J3" exist in JENDL-3⁴. Data of the nuclides with "x" are not given in JENDL-3, ENDF/B-VI nor JEF-2. The evaluation of the minor actinides for JENDL-3 has been reported elsewhere. ^{5,6} Data for ²³⁷U, ²³⁶Np and ²³⁸Np have been evaluated recently. Other evaluation will be completed by about 1997.

The data of the 7 **nuclides** with "A" will be taken from JENDL-3.2, which is the second revision of **JENDL-3**, without any modification. Those for the 13 **nuclides** of "B" will be based on JENDL-3.2 and some modifications will be made if needed. For the other minor actinides, the data of **JENDL-3.2** will be taken or new evaluation work will be made.

Jo the following sections, the evaluation work made so far for minor actinides is summarized, and as examples, the recently performed evaluation ${}^{237}_{10}\text{U}, {}^{236}_{10}\text{Np} \text{ and } {}^{28}_{10}\text{Np}$ is described.

A. Parameter for Theoretical Calculation

For the minor actinides, theoretical calculation is more important for the evaluation work because experimental data are so scarce. Theoretical calculation of cross sections and angular distributions of secondary neutrons were performed with a spherical optical and statistical model code CASTHY⁷ for most of minor actinides.

Optical Potential Parameters

Potential parameters most commonly used are as follows:

	Set 1	Set 2	Set 3
V	43.4-O.10	O7E V0-0.05E	41. 0-0.05E
$\mathbf{W}_{\mathbf{s}}$		339E 6.5+0.15E	6.4+0.15√E
	+0.0531E	\mathbb{R}^2	
V_{o}	7.0	7.0	7.0
r,r _o	1.282	1.32	1.31
rs	1.290	1.38	1.38
a, a _o	0.60	0.47	0.47
b	0.5	0.47	0.47

Their units are MeV for energy and fin for length. The parameters (Set 1) were determined so as to reproduce the total cross section of ²⁴¹Am⁸, and used to nuclides heavier than Am. Some alternatives were adopted for several nuclides. The parameters (Set 2) determined in Ref. 9, and those (Set 3) by Ohsawa and Ohta¹⁰ were used for U to Pu and nuclides lighter than Pa, respectively. The constant term of real potential (V0) of Set 2 is determined for each nucleus so that the calculation might reproduce the s-wave strength function estimated from experiments or systematic.

Level Density Parameters

A composite level density formula of Gilbert and Cameron¹¹ was adopted. The parameters were adopted from Ref. 10 or determined so as to be consistent with average resonance level spacing¹² and the number of low-lying excited levels¹³.

Level Scheme

Nuclear level scheme for inelastic scattering of each nucleus was determined on the basis of ENSDF^{13} or the Nuclear Data Sheets.

Table 1 Nuclides in JENDL Actinide File

nuclide_	status	nuclide	status	nuclide status
²⁰⁸ TI	X	²¹⁰ Pb	X	²¹⁰ Bi ×
$210_{_{\rm P0}}$	X	²²² Rn	×	²²³ Ra J3
$224_{\scriptscriptstyle Ra}$	J3	225_{Ra}	J3	²²⁶ Ra J3
$228_{\scriptscriptstyle Ra}$	X	225 _{AC}	J3	²²⁶ Ac J3
227 _{AC}	J3	227 _{Th}	J3	²²⁸ Th 13
²²⁹ Th	J3	230_{Th}	J3	²³¹ Th ~
232 _{Th}	J3,A	233 Th	J3	²³⁴ Th 13
229_{pa}	X	230_{pa}	X	231 p ₂ 13
$232_{_{pa}}$	J3	$233_{_{pa}}$	J3	2 3 0 ₀ ×
231_{u}	X	$232_{\scriptscriptstyle \mathrm{U}}$	J3	^{2 3 3} IT I3 A
$234_{\scriptscriptstyle U}$	J3	$235_{\rm u}$	J3,A	2 3 6 _{u 13}
237_{u}	New	$238_{\scriptscriptstyle U}$	J3,A	2 3 4 _{NP} ×
$235_{_{\mathrm{N}\mathrm{P}}}$	X	$236_{_{\mathrm{NP}}}$	•	^{2 3 7} N p J3.B
$238_{_{\mathrm{N}\mathrm{P}}}$	New,B	$239_{_{\rm NP}}$	J3	²³⁶ P ₁₁ 13
$237_{_{PU}}$,	$238_{\scriptscriptstyle PU}$	J3,B	²³⁹ Pu 13 A
$240_{_{PU}}$	J3,A	²⁴¹ Pu	J3,A	²⁴² p ₁₁ 13 R
$244_{_{\mathrm{PU}}}$	•	246 _{PU}	×	²⁴⁷ Pu x
²⁴¹ Am	J3,B	²⁴² Am	J3,B	^{242m} Am 13 B
²⁴³ Am	J3,B	²⁴⁴ Am	J3	^{244m} Am J3
²⁴⁰ Cm	×	²⁴¹ Cm	J3	²⁴² Cm 13 B
²⁴³ Cm	J3,B	²⁴⁴ Cm	J3,B	²⁴⁵ Cm 13 B
²⁴⁰ Cm	J3,B	²⁴⁷ Cm	J3	²⁴⁸ Cm 13
²⁴⁹ Cm	J3	²⁵⁰ Cm	J3	²⁴⁵ Bk ×
246 _{Bk}	X	2 4 7 _{вк}	X	²⁴⁸ Bk _×
²⁴⁹ Bk	J3	²⁵⁰ Bk	J3	²⁴⁶ Cf ×
²⁴⁸ Cf	X	²⁴⁹ Cf	J3	²⁵⁰ Cf 13
²⁵¹ Cf	J3	²⁵² Cf	J3	^ω 3 Cf 13
²⁵⁴ Cf	J3	$251_{\mathbf{Fs}}$	×	252 _{Fe} ~
253Es		254 _{Fs}	J3	^{254m} Es ×
²⁵⁵ Es	J3	255Fm	J3	

J3: data exist in **JENDL-3**, New: new evaluation for **JENDL** Actinide File has been completed, x: data are not existing in JENDL-3, **ENDF/B-VI** nor **JEF-2**, A: major actinide, B: important for the actinide burner reactor.

B. Resonance Parameters

In the low energy region, resolved resonance parameters were given on the basis of available experimental results. The parameters were adjusted so as to reproduce the thermal cross sections and resonance integral. Unresolved resonance parameters were determined with ASREP¹⁴ by fitting the fission and capture cross sections up to the energy around 30 keV.

C. Cross Sections

The fission cross sections were evaluated mainly on the basis of experimental data if available. If no experimental data were available, some **systematics**¹⁵ were used to estimate the cross section in the **MeV** region.

The (n,2n), (n,3n) and (n,4n) reaction cross sections for the minor actinides have not been measured. They were calculated with the simple evaporation model of $Pearlstein^{16}$ or Segev and $Caner.^{17}$

Calculation of the total, elastic and inelastic scattering and capture cross sections was made with CASTHY⁷. The fission and (n,Xn) reaction cross sections were considered as competing processes to the decay of the compound nucleus. The y-ray strength functions were determined with normalizing the capture cross section to the measured one in the 100-keV region.

D. Other Quantities

Angular distributions of elastically and inelastically scattered neutrons were also calculated with CASTHY.

Howerton's semi-empirical formula¹⁸ was adopted for the number of prompt neutrons per fission, and Tuttle's systematics¹⁹ for delayed neutrons. If the measured data were available, they were adopted.

Evaporation spectra were given for the neutrons due to inelastic scattering to the continuum region and (n,Xn) reactions. The nuclear temperature was estimated from the level density parameters. For fission neutrons, evaporation spectra were also adopted with temperature mainly based on the systematic by Smith et al. 20

E. Evaluation of Uranium-237 Data

Resonance parameters from 46 to 200 eV were determined from the fission area data measured by McNally et al. ²¹ They measured the ²³U fission cross sections by using neutrons from an underground nuclear explosion (Pommard). Below 46 eV, hypothetical levels were generated by assuming level spacing of 3.5 eV²¹, the s-wave strength function of 1 x 10⁴, Γ_{γ} of 35 meV and Γ_{f} of 4 meV obtained from the data of McNally et al. ²¹ Parameters of a negative level and low-lying levels were adjusted so as to reproduce the thermal fission cross section of about 2 b²² the. absorption cross section of 478 \pm 160 b²³ and capture resonance integral of 1200 \pm 200 b²⁴. An effective scattering radius of 9.38 fm was obtained from the optical model calculation. Unresolved resonance parameters were determined on the basis of cross sections up to 30 keV.

The fission cross section in the MeV region was based on a calculation with a simple formula by Bychkov et al. 25 , experimental data by Cramer and $Britt^{26}$ and systematic by Behrens and Howerton. 15 The fission cross section from 200 eV to 100

keV was interpolated from 2.5 b at 200 eV and 0.6 b at 100 keV.

The (n,2n) and (n,3n) reaction cross sections were calculated with the formula by Segev and Caner 17 by considering the fission cross section determined above. The (n,4n) reaction was ignored. Therefore the present result of the (n,3n) cross section above 17 MeV could be too large.

The total, elastic and inelastic scattering and capture cross sections were calculated with CASTHY. The optical potential of Set 2 was adopted with VO of 40.5 MeV that reproduces the s-wave strength function of 1 x 10^{-4} . The average level spacing of 3.5 eV 21 and Γ_{γ} of 35 meV were assumed. The fission, (n,2n) and (n,3n) reaction cross sections described above were taken into account as competing processes to the decay of compound nucleus of ^{238}U .

The fission cross section is compared in Fig. 1 with END-F/B-VI.²⁷ Below 200 eV, the cross sections **in** the figure are mean values in suitable energy intervals. The cross section is largely discrepant in the resonance region because the present evaluation adopted the experimental results of McNally et al., whereas ENDF/B-VI are not based on the experimental data but on hypothetical resonances. According to our experience, the fission cross sections measured with underground nuclear explosions are often to be too large. The data of McNally et rd. also might be too large but we have no other **experimental** data for this cross section. The other cross sections are shown in Fig. 2.

The thermal cross sections and resonance integral are listed in Table 2. Large discrepancies are found in the resonance integral between the present results and ENDF/B-VI.

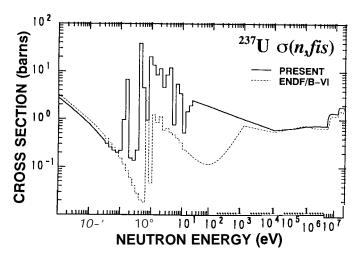


Fig. 1 The fission cross section of ²³⁷U. Data below 200 eV are mean values in energy bins.

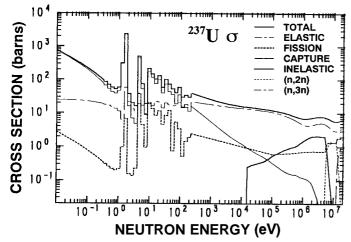


Fig. 2 Cross sections of 237U. Data below 200 eV are mean values in energy bins.

Table 2 Thermal cross sections and resonance integral of ²³⁷U

2200m/sec a(b) present ENDF/B-VI			σ _{ela} 24.39 9.13	σ _{tot} 478.5 487 _, 1	
Resonance integral (I present ENDF/B-VI	o)	σ _{cap} 1080 311		σ _{fis} 48.7 9.22	

F. Evaluation of Neptunium-236 and -238 Data

No resolved resonance parameters have been measured for these two **nuclides**. Since the level spacings (0.11 eV for ² 029 eV for ²³⁸Np) estimated from their level densities are very small compared with average fission widths (about 0.4 eV²⁸ for ²³⁶Np), strong overlapping of resonances can be expected. Therefore no resonance parameters were given to these two

The fission cross section of ^{236}Np was based on the data measured by Val'skiy et al. 28 below 20 keV. The capture cross section in this energy region was determined by assuming the capture-to-fission ratio of 0.253 that was estimated from the CASTHY calculation at 20 keV. The fission cross section of ²³⁸Np was assumed to be in the form of 1/v and 2070 b²⁹ at 0.0253 eV. The capture cross section was calculated with CASTHY.

The fission and (n,Xn) reaction cross sections above 20 keV were estimated with the same method as ^{237}U . Other cross sections were calculated with CASTHY by using the same optical potential parameters ²äU The y-ray strength functions were obtained from Γ_{ν} of 35 meV and the above-mentioned level

The thermal cross sections and resonance integral are listed in Table 3. The cross sections of $^{236}{\rm Np}$ and $^{^{238}}{\rm Np}$ are shown in Figs. 3 and 4.

Thermal cross sections and resonance integral of ^{236}Np and ^{238}Np Table 3

	²³⁶ Nn		2 3 8 _{Nn}
2200m/sec σ (b) present ENDF/B-VI	σ _{cap} 701	σ _{fis} 2770	$ \begin{array}{ccc} \sigma_{\text{cap}} & \sigma_{\text{fis}} \\ 450 & 2070 \\ 202.8 & 2026.9 \end{array} $
Res. integ(b) present ENDF/B-VI	σ _{cap} 259	$\sigma_{ m fis}$ 1030	σ _{cap} σ _{fis} 201 940 100 898

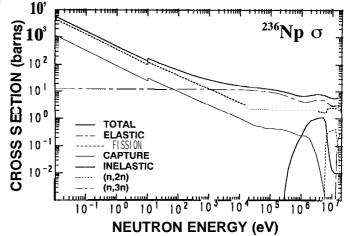


Fig. 3 Cross sections of ²³⁶Np.

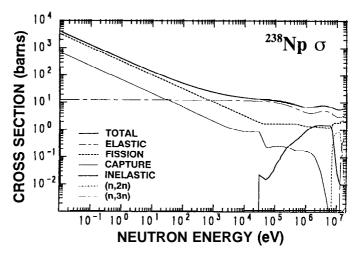


Fig. 4 Cross sections of ²³⁸Np.

G. Future Work for Class B **Nuclides**Among the **class** B **nuclides**, ²³⁷Np, ²³⁸Pu, ²⁴¹Am and ²⁴³Am are the main fissile nuclides which sustain the chain reactions in the actinide burner reactor. Hence more accurate data are required for the fission and capture cross sections, v-values and delayed neutron data. Particularly, the inventories of 237Np and ²³⁸Pu are large, and their inelastic scattering cross sections affect the reactor spectrum. The direct inelastic scattering should be taken into account for them.

IH. EVALUATION FOR HIGH ENERGY DATA FILES

Two high energy data files will be produced; one includes the neutron nuclear data in the energy range up to 50 MeV and another file the neutron— and proton-induced reaction data up to 1.5 GeV. The file up to 50 MeV will supply the neutron data for the ESNIT project of JAERI. In this energy range, the evaluation method similar to the evaluation below 20 MeV can be adopted. The latter file up to 1.5 GeV is planned to support the design of the accelerator-driven spallation system. The data provided in this file are those of structural materials of the system, candidates of the spallation targets (W, Pb, Bi), and nuclides to be transmuted. These two files will be compiled in the ENDF–6 format. In this Chapter, the typical method of the nuclear data evaluation for the file up to 1.5 GeV is explained using the results of evaluations for the file up to 1.5 GeV and geven to 1.0 GeV.

A. Total and Reaction Cross Sections

Total and total reaction cross sections are basic quantities of nuclear data evaluation. They can be obtained by optical. model calculation with a global potential derived by Pearlstein or estimated from Pearlstein's systematic. 30 The 'latter was mainly used in the evaluation of Al, Pb and Bi. The evaluated result of neutron total cross section for pb with Pearlstein's systematic is compared with experimental data in Fig. 5. The evaluated result reproduces the overall trend of the experimental data well.

B. Isotope Production Cross Sections

The isotope production cross sections are the total residual **nuclide** production cross sections integrated over all charnels of reactions. They were mainly evaluated by using a multi-step compound decay model code with **precompound** correction, **ALICE-F**, ³¹ which is a modified version of ALICE/89. ³² The main improvements **from** ALICE/89 are the following

- 1) The **preequilibrium** cluster particle emission is considered for d, t, ³He and a with **Iwamoto-Harada** cluster formation **model**^{33,34} in order to reproduce spectra in the high energy region of the emitted cluster particles.
- 2) The latest mass formula derived by **Tachibana** et al.³⁵ is added for binding energy calculation.
- 3) The y-ray incident reaction can be treated.

The calculated result of the ²⁷Al(p,x)²⁴Na reaction cross section is shown in Fig. 6 with the experimental data. Although the calculation was performed with the default parameters of ALICE-F, the result follows the trend of experimental data.

C. Double Differential Particle Emission Cross Sections

The DDXS were basically **evaluated** with the semi-empirical formulas which were derived by **Pearlstein** for **neutrons**³⁶ and by **Kalbach** for charged particles. Kalbach's formula needs **angle**-integrated particle spectra and the ratio of the component for multi-step direct process to that for total emission. They were mainly calculated by the ALICE-F code.

D. Fission Cross Section

For heavier elements than silver, the fission cross section is

not negligible in the energy region above a few hundred MeV. The proton-induced fission cross section was obtained by the following empirical formula derived by **Fukahori**:³⁸

$$\sigma_{fs}[mb] = PI_{X}(I - \exp(-P2 \times (E_p - P3))), \tag{1}$$

where

and $X=Z^2/A$, $Y=A^{2/3}$, E_p is the incident proton energy in MeV, Z and A the atomic and mass numbers of the target nuclides. For the neutron-induced fission, the cross section is estimated to be a half of Eq. (1) as a result of comparison with several sets of experimental data. The calculated result of proton-induced fission cross section for ^{209}Bi is compared with the experimental data in Fig. 7.

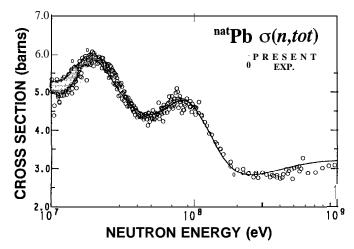


Fig. 5 The total cross section of ²⁰⁸Pb.

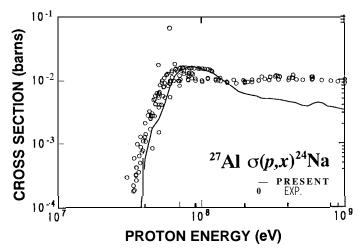


Fig. 6 The ²⁷Al(p,x)²⁴Na reaction cross section.

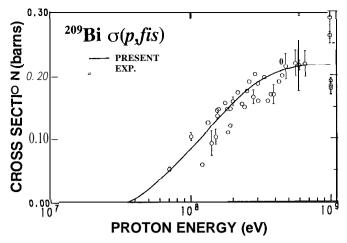


Fig. 7 The fission cross section of ^{209}Bi .

E. New Evaluation Methods for High Energy Files

The examples of data evaluation in the intermediate energy region outlined above is mainly based on the phenomenological models. However, these methods are not free from a lot of adjustable parameters, and therefore reliability of their results is not certain, especially when they are applied to the energy region where the parameters have not been examined. Moreover, they do not consider the final channels including n-meson and other elementary particles, and such exotic reactions as multi-fragmentation are not treated explicitly. In order to solve these problems, new techniques, based on more microscopic description of the nuclear process, will be investigated and developed which are going to readopted intheevaluation forthefile up to 1.5 GeV.

For example, the nucleon total, elastic and reaction cross sections are known to be well described by the relativistic impulse approximation (RIA)³⁹in theenergy region above around 100 MeV. Figure 8 gives the total and reaction cross sections of Pb, where the solid crirves give the predictions with RIA. The RIA was proved to be a powerful tool to give a consistent description of the total, elastic (including angular distribution) and reaction cross sections in this energy region. The reaction cross section calculated in this way can be then used to normalize the results obtained by other methods, such as those described below.

The reaction part of the cross section can recalculated bya microscopic simulation method such as the cascade model⁴⁰ and Quantum Molecular Dynamics (QMD).⁴¹ These methods are considered to be vital tools in calculating the cross section in the intermediate energy region because of their flexibility in including N–Nonelastic channels, fission, dynamical fragmentation, and so on. In this approach, an extension of the NMTC/JAERI code⁴² is being planned; 1) it will be rewritten to a full cascade program, 2) cross sections of the basic nucleon-nucleon reaction will be updated by taking account of the present phase-shift analysis, and 3) number of inelastic channels will be increased. Next, the effects of the nuclear mean field will be taking account according to the concept of QMD; a nucleon will be expressed by a Gaussian wave packet. Between two nucleon-nucleon collision, it will move according to the Newtonian equation. In this way,

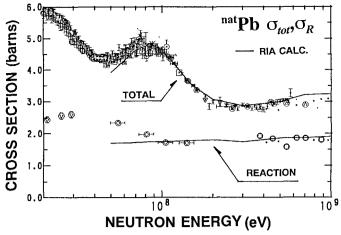


Fig. 8 The Pb total and reaction cross sections calculated with RIA.

the nucleon motion and nuclear mean field can be calculated in the self-consistent manner, By normalizing the event number versus **total** history of QMD to the reaction cross section **calculated** by RIA, the reaction can be described in a folly microscopic way. This approach will be applied in the evaluation work for the high energy file up to 1.5 GeV.

IV. CONCLUDING REMARKS

The present status and plans of the JENDL Actinide File and high energy files were shortly described. The JENDLActinide File will provide the neutron-induced reaction data for 89 nuclides from ²⁰⁸Tl to ²⁵⁵Fm in the energy range from 10⁵ eV to 20 MeV. The evaluation for 61 nuclides out of 89 has been finished. Wehaveto make new evaluations for 28 nuclides. For lack of experimental data forthese minor actinides, the evaluation of large part of the data will be based on calculations. Advanced methods will be investigated for this. Furthermore, some modifications of existing evaluated data will be also made especially for important nuclides.

The high energy files will store the data needed for **ESNIT** and for the accelerator-driven **spallation** system. Examples of typical **evaluation** method and results for the file up to 1.5 **GeV** were shown in this paper. The evaluation for the high energy data files will be made with the method described in Sections A to D of Chapter III. Reliability of these methods were confirmed. However, for most of **nuclides**, available experimental data are not enough for the evaluation and for checking reliability of the evaluation methods. Therefore more careful theoretical **calculations** are desirable. The method given in Section E of Chapter III will be also applied to the evaluation.

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